

Detection of gait perturbations based on proprioceptive information. Application to Limit Cycle Walkers

J.A. Gallego^{a,*}, A. Forner-Cordero^b, J.C. Moreno^a, E.A. Turowska^a and J.L. Pons^a

^a*Bioengineering Group, Consejo Superior de Investigaciones Científicas, CSIC, Arganda del Rey, Madrid, España*

^b*Biomechanics Laboratory, Mechatronics and Mechanical Systems Department, University of Sao Paulo, Sao Paulo, Brazil*

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Abstract. Walking on irregular surfaces and in the presence of unexpected events is a challenging problem for bipedal machines. Up to date, their ability to cope with gait disturbances is far less successful than humans': Neither trajectory controlled robots, nor dynamic walking machines (Limit Cycle Walkers) are able to handle them satisfactorily. On the contrary, humans reject gait perturbations naturally and efficiently relying on their sensory organs that, if needed, elicit a recovery action. A similar approach may be envisioned for bipedal robots and exoskeletons: An algorithm continuously observes the state of the walker and, if an unexpected event happens, triggers an adequate reaction. This paper presents a monitoring algorithm that provides immediate detection of any type of perturbation based solely on a phase representation of the normal walking of the robot. The proposed method was evaluated in a Limit Cycle Walker prototype that suffered push and trip perturbations at different moments of the gait cycle, providing 100% successful detections for the current experimental apparatus and adequately tuned parameters, with no false positives when the robot is walking unperturbed.

Keywords: Perturbation detection, dynamic stability, bipedal robots, Limit Cycle Walking, basin of attraction

1. Introduction

Research on gait synthesis constitutes a constructive manner to increase our understanding of the principles underlying human walking. This knowledge is useful in two types of applications: human-centered applications, and robotics-centered applications. The former include the design of improved rehabilitation devices such as robotic exoskeletons or prostheses, Pons [23], Au and Herr [3], whereas the latter will translate into the development of humanoid robotic companions and caretakers, entertainment robots, and social interaction robots in general, Sakagami et al. [27], Ishida [16].

Unfortunately, taking these systems from the labs to our daily context is yet not entirely possible, because our real world is full of non expected events that may lead the walker to a fall, e.g. obstacles, ground irregularities, slope changes, and collisions with other robots or humans. Therefore, recovery from gait perturbations and balance control emerge as major topics in bipedal walking.

Concerning to the rejection of perturbations, humans cope with this problem in a quite successful manner choosing among a reduced repertoire of strategies, which are adapted to the specific context, Schillings et al. [28], Forner-Cordero et al. [10]. When a perturbation takes place, multiple sensory receptors trigger a certain reaction, trying to avoid a fall, Eng et al.

*Corresponding author. E-mail: gallego@iai.csic.es.

[8]. In fact, stumbling reactions or biological recovery motions to keep the human body stable during walking, are -partially-modulated by peripheral afferent signals, Duysens and van deCrommert [7]. Thus, kinesthetic information needs to be fed back in order to update the central motor program, which can be regarded as a modulated closed system, Llinás [20]. Considering this, it seems interesting to investigate a similar solution for robotic walkers and exoskeletons: An algorithm continuously monitors the state of the biped and, if necessary, triggers a recovery reaction. This is the final objective of EU project ESBiRRo (IST-61-045301-STP), which aims at developing biomimetic recovery reactions for gait control that will be implemented into an autonomous biped robot and a robotic exoskeleton. This paper focuses on a general method for detection of any type of external gait perturbation in robotic walkers.

It is hypothesized that the human cerebellum generates a series of forward and inverse models, which represent the normal behavior of the motor system in response to ongoing motor commands, and the neural command required to generate a given trajectory respectively, Wolpert et al. [32]. Regarding to forward representations, different structures and/or functions are attributed to them, such as output prediction, state estimation or distal teaching, Kawato [18]. Functional brain imaging studies signal that the cerebellum is involved in signalling the discrepancy between the predicted and actual sensory consequences of movement Blakemore et al. [5]. Moreover, in a recent work, Ahmed et al. [1], it is hypothesized that a nominal forward internal model combined with probabilistic error monitoring is employed by the Central Nervous System to detect a loss of balance and precedes any observable compensatory response.

On the other hand, gait synthesis as understood in the framework of Limit Cycle Walking, relies on keeping in the neighborhood of the limit cycle prescribed by the robot state during a stride. Indeed, it has been proven that optimization of the system dynamics makes exponentially stable, efficient, and natural gait emerge, Westervelt et al. [31], and that simple torque control provides the biped with the ability to cope with varying walking speeds, ground slopes, and push perturbations, Braun and Goldfarb [6]. This happens because the limit cycle prescribed by a system is enveloped by a surface known as basin of attraction, which contains all the states that bring the system “naturally” back to its limit cycle. However, the basin of

attraction is not analytically computable for systems with such a large number of state variables as a walking robot, Strogatz [29]. According to this, the problem of detecting whether the walker is undergoing or not a perturbation that will lead to a fall equals to estimating whether it is inside or outside the basin of attraction.

On the basis of these two ideas, we propose a method for instability detection in Limit Cycle Walkers, which consists in estimating the deviation between the actual and expected robot state as provided by sensory signals, to subsequently compare it with a linear, probabilistic approach to the basin of attraction.

Regarding to the state of the art, research on perturbation detection in biped robots has focused on tailor made techniques, which detect a well defined perturbation in order to implement some reflex, recovery strategy, or balance control mechanism to avoid a fall. In Nakanishi et al. [21], a method to detect a push in the trunk by observing the upper body acceleration in the antero-posterior direction is proposed. In a more recent work, Prahlad et al. [24], they implement ankle control to permit a small walking robot adapting to both continuous perturbations (slope changes, addition of mass) and pushes. The latter are simply detected with a force sensor attached at the back of the robot.

Looking at more general detection and classifications paradigms, an algorithm to predict the fall of a prototype due to moderate ground irregularities is proposed in Karssen and Wisse [17]. This method relies on monitoring the whole state of the robot and is validated with a limit cycle prototype, providing successful detection in the last heel strike before the fall. A method for instability detection during omnidirectional walking to trigger a reflex mechanism is proposed in Renner and Behnke [26]. Perturbations are classified in one of two groups according to their strength, and a different reflex is executed based on this identification. The method is validated with a real prototype that stumbles over a wall. In Höhn and Gerth [14] a probability based algorithm is employed to classify the robot state in viable (i.e. keep walking), perturbed (a reflex mechanism may avoid the fall) or unavoidably leading to a fall. A similar approach is presented in Ogata et al. [22] where the mean deviation from normal walking during a whole step is employed to activate a shock-reducing motion if a fall is foreseen.

This paper is organized as follows: first the method for detection of perturbations in robotic walkers is described. Next Section 3 presents an example of application in the real prototype, whereas Section 4

includes the discussion and an outline of future research. Finally, some conclusions summarizing the main results are provided.

2. Detection of perturbations based on the Nearest Neighbor Gait Index

This section describes a novel algorithm for perturbation detection in robotic walkers. It is based on a normal walking pattern, allowing for real-time implementation and negligible detection delay.

The algorithm is executed in two steps, Fig. 1. First, it calculates the state in a normal walking pattern (the Reference Limit Cycle, RLC) that best represents the real state of the robot (what we call the Nearest Neighbor Gait Index, NNGI), and afterwards it computes the (weighed) deviation between this expected state and the actual state of the walker. The weighed deviation (D-statistic) provides an experimental approximation to whether the robot is inside or outside the basin of attraction based on a threshold.

Before running the algorithm, the normal walking of the robot, the Reference Limit Cycle, must be defined offline. Afterwards, during its execution, the first part of the algorithm, the application of the NNGI is subdivided in two steps: 1) the selection of a subset of possible states in the RLC, the Ensemble of Candi-

date Neighbors (ECN), in order to save computational burden, and 2) the search of the point within the aforementioned subset that represents best the current state of the walker, the Selection of the Nearest Neighbor (NN), Fig. 1. As said, during the second step, the algorithm computes the weighed distance between the NN and the current state of the walker (Section 2.2). Comparing it with a threshold corresponds to a linear approach to being inside or outside the basin of attraction. The complete procedure is described in detail in the next paragraphs.

2.1. The Nearest Neighbor Gait Index (NNGI)

The NNGI looks for the state in the normal walking pattern, the RLC, that matches best the current state of the robot.

2.1.1. Definition of the Reference Limit Cycle (RLC)

The RLC provides the normal walking of the biped. It is obtained off-line by averaging a series of stable runs on a surface with small disturbances. The disturbances should be large enough to cause variation between strides (cycles) without making the robot collapse. Notice that an analytical frontier between small and large perturbations cannot be established, because the former are those that do not make the

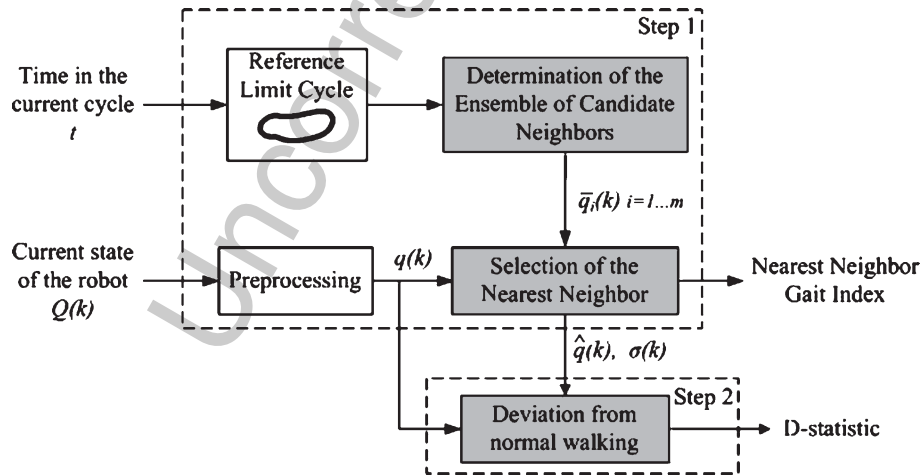


Fig. 1. Block diagram summarizing the proposed method. First the current state of the walker $Q(k)$ is processed to obtain $q(k)$. Afterwards, based on timing information, an Ensemble of Candidate Neighbors (ECN) is selected. The ECN is a subset of the Reference Limit Cycle that represents the normal walking of the robot. Next a Nearest Neighbor search to find the state in the ECN that matches best the current state of the robot, $\hat{q}(k)$, is performed. Finally, the deviation between the expected and current state of the walker is calculated, the D-statistic. This constitutes, together with the NNGI, the output of the algorithm.

walker collapse whereas the latter do, and this would require computing analytically the basin of attraction, which is, as stated above not possible for a Limit Cycle Walker. Hence, we consider a perturbation to be small if it causes no (even visually) remarkable deviation from the normal gait pattern on flat terrain. In practice, small perturbations during calculation of the RLC are applied by making the biped walk on a carpeted floor, which light irregularities may be assimilated to white noise.

Because of the underactuated nature of Limit Cycle Walking, inter-stride variations in both duration and joint trajectories (and velocities) take place, Hobbelen and Wisse [11]. Therefore, to obtain the RLC the first step is to scale joint angles and angular rates to stride percentage. Next, to take the range of each joint into account and to avoid problems related to units, phase variables (joint angles and angular rates) $Q_j(k)$, $j = 1, \dots, 2n$ are divided by their respective maxima, $\max(|Q_j|)$, $j = 1, \dots, 2n$, (1). Like this, RLC variables at every instant k vary within $[-1,1]$. It must be noted that the resultant scaled phase space is unbounded, i.e. any variable can be outside the $[-1,1]$ interval, for example, when the robot suffers a perturbation.

$$q_j(k) = \frac{Q_j(k)}{\max(|Q_j|)} \quad (1)$$

Once phase variables have been averaged to percentage and scaled, the $2n$ -dimensional RLC is obtained as the mean trajectory \bar{q} of each variable for the p recorded strides, (2). The standard deviation σ of each variable at each point of the RLC is also calculated, (3), because it will be used in the measure of deviation. Afterwards $\bar{q}_j(k)$ and $\sigma_j(k)$ are resized to a number of samples that corresponds to the average duration of a stride, r . Note that the mean stride duration will provide an estimate of the state in the RLC that corresponds to the current state of the walker as will be discussed below.

$$\bar{q}_j(k) = \sum_{j=1}^p \frac{q_j(k)}{p}, \quad k = 1, \dots, 100 \quad (2)$$

$$\sigma_j(k) = \left(\frac{1}{p-1} \sum_{j=1}^p (q_j(k) - \bar{q}_j(k))^2 \right)^{1/2}, \quad k = 1, \dots, 100 \quad (3)$$

2.1.2. Determination of the Ensemble of Candidate Neighbors (ECN)

Limit Cycle Walking is a nominally periodic sequence of strides, which means that in the absence of (large) perturbations each stride is almost an exact mapping of the previous one, Hobbelen and Wisse [11]. Therefore at time t in step number s , the walker will be in a state very close to the the one it was in at time t during step $s - 1$. Assuming this, in order to look for the state of the RLC at which the robot is at time t , we can select an interval of m points (the Ensemble of Candidate Neighbors, ECN) around the expected state at time t : If the robot has not suffered a disturbance its state will be within this interval. This is illustrated in Fig. 2: the walker is in the state $q(k)$ and the algorithm expects it to be in the plotted interval based solely on time information. However, if the walker has undergone a perturbation, it will deviate very quickly from its expected state. The convergence time of the NNGI is equal to the number of samples of the RLC, r , divided by the length of the ECN, m . This is the first (out of two) parameter the designer has to adjust.

It must be noted that disturbances in limit cycles can be assessed in the directions tangential and transverse to the cycle, i.e. we can distinguish between those perturbations that make the system “advance” (or “go back”) in the limit cycle, and those that cause a deviation in an orthogonal manifold, Ali and Menzinger [2]. Therefore, if the ECN is too long the algorithm will not detect perturbations that manifest in an abrupt change in the tangential direction, or it will detect them slower than with an ECN that comprises less states. Subsection 3.2 summarizes the tuning process for a Limit Cycle Walking prototype.

2.1.3. Selection of the Nearest Neighbor (NN)

The last part of the NNGI consists of finding the state of the RLC that matches best the current state of the walker. In order to reduce computational cost, and because during normal walking the correspondent state must be within the ECN, we perform a Nearest Neighbor (NN) search on there. The NN algorithm is a widely extended method for finding closest points in Euclidean spaces: it will provide directly the most similar state in the normal walking pattern. It has already been applied in off-line analysis of human gait, Forner-Cordero et al. [10].

The NN, $\hat{q}(k) = \hat{q}_j(k)$, $j = 1, \dots, 2n$ at sample k is simply defined as the point within a metric space (the m points \bar{q}_i , $i = 1, \dots, m$ in the ECN subset in our

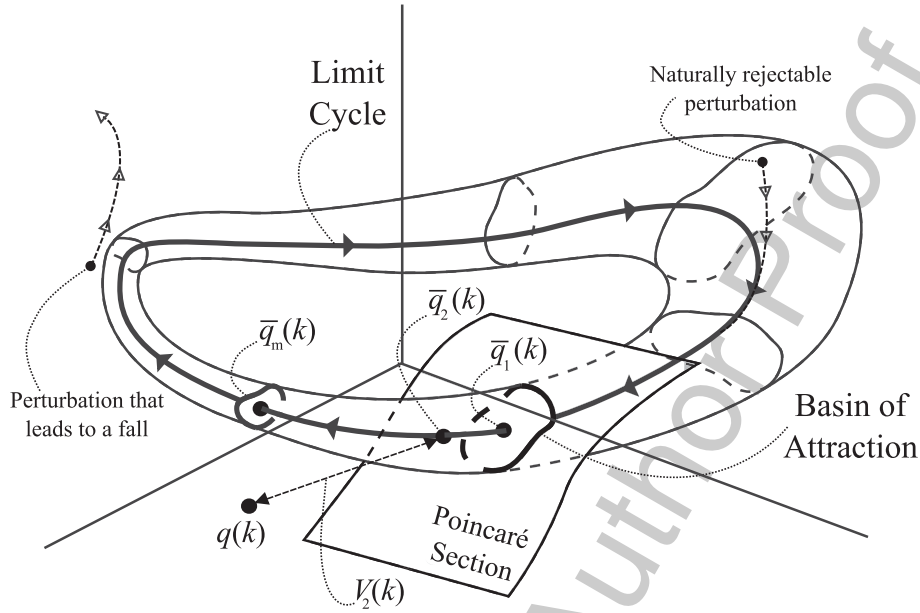


Fig. 2. 3-Dimensional abstraction of a limit cycle (solid line) together with its basin of attraction (enveloping surface). The Ensemble of Candidate Neighbors (ECN) is represented as slices in the limit cycle.

case) with the least Euclidean distance $V_i(k)$ to the query point, obtained after preprocessing the state of the walker with equation 1, $q(k) = q_j(k)$, $j = 1, \dots, 2n$, (4), (5).

$$V_i(k) = \left(\sum_{j=1}^{2n} (q_j(k) - \bar{q}_{j,i}(k))^2 \right)^{1/2}, \quad i = 1, \dots, m \quad (4)$$

$$NN(k) = \min\{V_1(k), V_2(k), \dots, V_m(k)\} \quad (5)$$

2.2. Calculation of the deviation from normal walking

Once the NNGI has been selected $\hat{q}(k)$, the state in the RLC most similar to the actual state of the biped, $q(k)$, a perturbation may be detected by measuring their relative distance and estimating whether the walker is inside or outside its basin of attraction. However, the selection of an adequate measurement is not straightforward. It must be considered that a given amount of deviation does not have the same effect on dynamic stability if it takes place in different variables (i.e. processed joint angles or velocities) or even at different

gait phases because the basin of attraction changes its shape and size at every point of the limit cycle. Therefore a good metric must include different weights for each variable and time instant.

The D-statistic proposed in Karssen and Wisse [17] takes both aspects into account. It consists in the squared error (between the actual and expected state of the robot) weighed by the standard deviation at that instant and variable, (6). The standard deviation quantifies the variability of a given variable during normal gait, which is related to the basin of attraction. The idea is to select a threshold for the D-statistic that separates the stable and unstable walking regions of the phase space, D_{th} , mimicking the basin of attraction. This is the second parameter the designer has to tune, subsection 3.2. Note that if the designer chooses a small value for D_{th} , the algorithm will detect perturbations that could be rejected naturally, but if its too large, it will fail to detect that the robot is being perturbed, or it will not provide a sufficiently fast detection.

$$D(k) = \frac{1}{2n-1} \sum_{j=1}^{2n} \frac{1}{\sigma_j(k)^2} (q_j(k) - \hat{q}_j(k))^2 \quad (6)$$

where $(q_j(k), \hat{q}_j(k))$, $j = 1, \dots, 2n$ stand for the current state of the biped and its NN respectively. $\sigma_j(k)$

333 is the standard deviation of each RLC variable \hat{q}_j at
 334 sample k .

335 2.3. Interpretation of the algorithm

336 The algorithm proposed in this paper provides two
 337 output variables that are interesting to evaluate the
 338 dynamic stability of a walker. On the one hand, the
 339 NNGI relates the actual state of the biped to one state
 340 in its average limit cycle, the RLC. On the other hand
 341 the D-statistic is a weighed measure of the deviation
 342 between them and constitutes a linearized estimate
 343 of the basin of attraction. They can be plotted as in
 344 Fig. 3. The upper panel shows the NNGI (dashed line)
 345 and the RLC (solid line). When the robot is
 346 walking stably the NNGI will track the RLC very
 347 closely (two first strides in the figure). However, if it
 348 suffers a perturbation the NNGI will deviate as hap-
 349 pens in the third stride. The lower panel provides the
 350 D-statistic (solid line), the deviation measurement. Its
 351 interpretation is straightforward: The larger it is, the
 352 further the robot is from its limit cycle. Based on a
 353 series of stable and perturbed walking experiments
 354 the designer can select a threshold for the D-statistic
 355 (D_{th} , dashed line) that establishes whether the robot
 356 is about to suffer a fall, or it will continue walk-
 357 ing stably, mimicking the concept of the basin of
 358 attraction.

359 3. Evaluation of the NNGI for detection of 360 perturbations in a Limit Cycle Walker 361 prototype

362 This section presents the evaluation of the proposed
 363 technique with a Limit Cycle Walker prototype. After
 364 an overview of the robot, we summarize how the
 365 parameters of the algorithm were selected. At last,
 366 experimental results of stable and perturbed walking
 367 are provided.

368 3.1. System overview of Meta

369 Meta is a “four-legged biped” developed at Delft
 370 University of Technology, Hobbelen and Wisse [12].
 371 Mechanical coupling between inner and outer leg pairs
 372 makes it walk in an almost straight line, i.e. the dynamic
 373 behavior of the walker is almost two-dimensional. The
 374 prototype has seven body parts (an upper body, two
 375 upper legs, two lower legs, and two feet) and the same
 376 amount of DoF, located at the body (external DoF),
 377 hips, knees, and ankles, Fig. 4a.

378 Meta has four powered DoF, both ankles and hips,
 379 actuated with DC motors placed close to the hip. This
 380 configuration keeps the limbs inertia low. Series Elastic
 381 Actuation interfaces ankle joints with their actuators,
 382 Pratt and Williamson [25], reducing the interface stiff-
 383 ness, enhancing shock tolerance and decreasing the

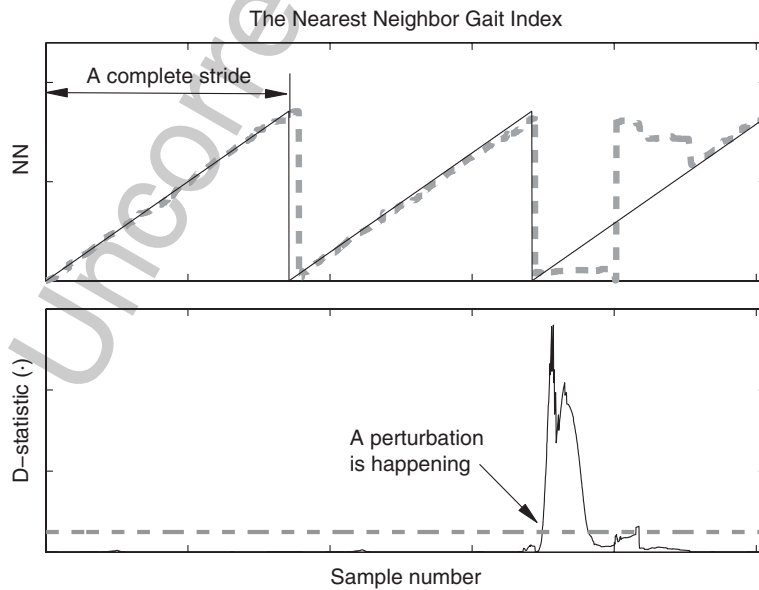


Fig. 3. An example of the execution of the proposed method. The upper panel shows the NNGI (dashed line) and the RLC (solid line). The lower panel shows the D-statistic (solid line) and its threshold D_{th} (dashed line).

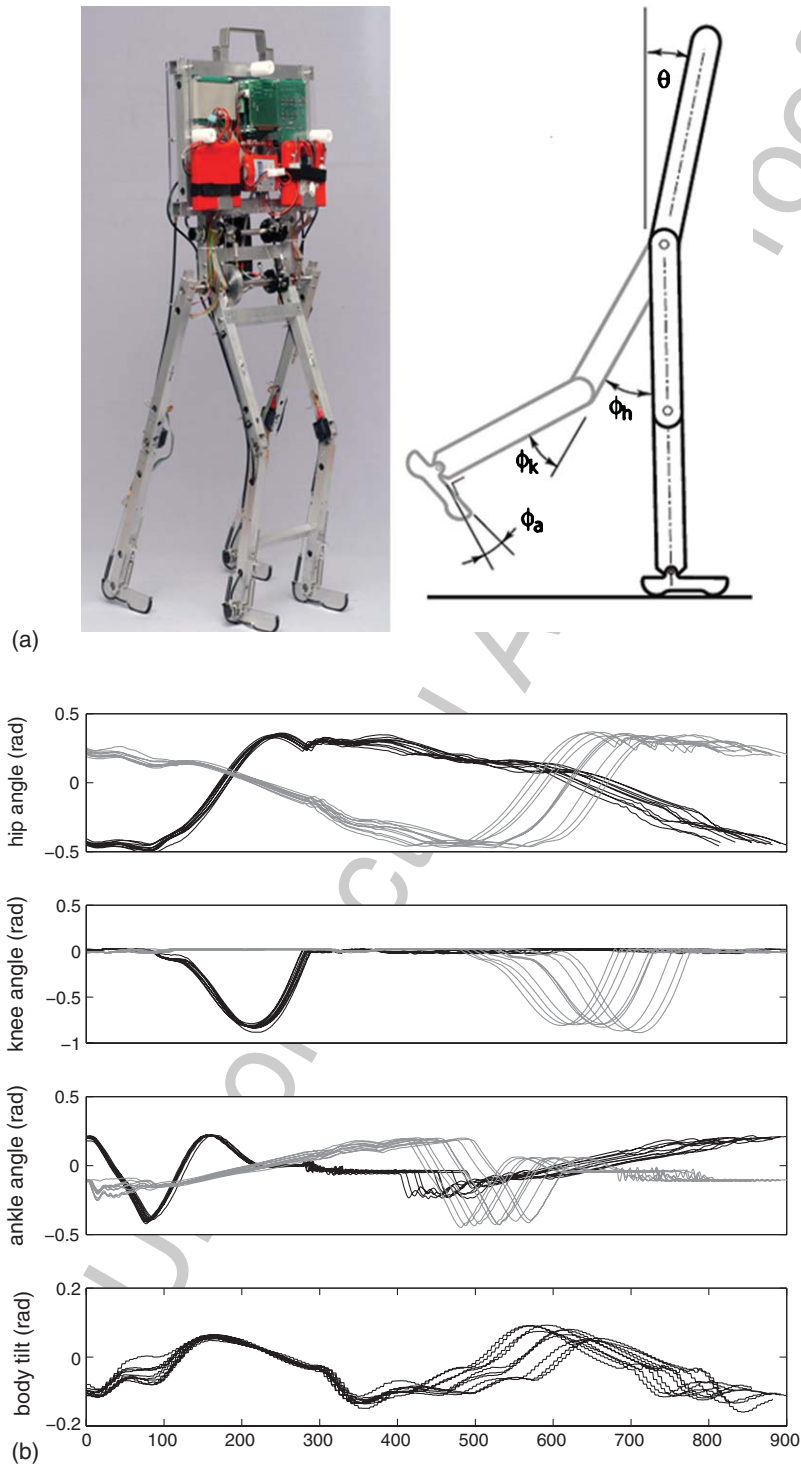


Fig. 4. Limit Cycle Walker Meta: Appearance, schematic representation, and joint angles during normal walking. (a) Appearance and schematic representation depicting the DoF of Meta. Because of the coupling between the inner and outer pairs of legs the walker may be thought of as two dimensional. (b) Joint angles (rad) for the hip, knee, ankle, and body tilt of 10 (out of 28) strides employed to calculate the RLC of Meta. Data sampled at 500 Hz. The black and grey lines represent the inner and outer legs respectively.

amount of reflected inertia. Moreover, ankle joints can be torque controlled measuring the elongation of the elastic element. The passive knees are equipped with a solenoid-driven latch which unlocks the knee at the start of the swing phase.

Angles of the six joints are measured with incremental encoders. They provide a resolution of 4×10^{-4} rad for the hip, 3×10^{-4} rad for the knee, and 2×10^{-4} rad for the ankle joints. Body tilt is obtained with a vestibular organ that consists of three accelerometers and three gyroscopes. Ground contact is detected by one switch placed underneath each foot. Sensory data is sampled at 500 Hz rate. Meta is controlled with a PC/104 stack that includes a 400 MHz processor. The gait controller consists in a state machine that provides both feedback and feedforward commands.

3.2. Preliminary calculations and selection of parameters

Limit Cycle Walkers rely on reduced sensory information for gait control. Usually, as in Meta, angular rate is obtained by numeric differentiation of the encoder signals employed to measure joint angles, a procedure that amplifies high frequency noise. Considering that limit cycle walking requires low bandwidth, high frequency noise can be removed by low-pass filtering. To allow for fast detection of perturbations the filter selected must introduce no delay. We have chosen the Benedict-Bordner filter, a tracking algorithm that provides an optimal trade-off between signal smoothing and tracking, Benedict and Bordner [4], because achieves good filtering with zero phase.

Before running the NNGI, the normal walking pattern of the robot (RLC) must be obtained. In this case we made Meta walk 14 runs on a carpet, Fig. 4b. Only two of the last strides of each run were considered to avoid transient effects. Signals were processed as described in Section 2.2.1 and next joint velocities were Benedict Bordner filtered; afterwards the RLC and its standard deviation for a stride of average duration, 1.71 s (standard deviation 0.073s), were obtained. The RLC has a length $r = 855$ samples at 500 Hz.

As explained above, the perturbation detection method has two parameters that need to be tuned because they depend on the characteristics of the robot. These parameters are:

- The length of the Ensemble of Candidate Neighbors (ECN), m . The number of states within the

ECN is related to the inter-stride variability, and depends on the duration of a complete stride, the sensors sampling rate, and the capability of the onboard computer of the walker. As said in Section 2.1.2, if m is too large the algorithm may ignore the occurrence of a perturbation, while if it is too small it may provide false positives. Figure 5b shows an example of the influence of m : If $m \geq 60$ the algorithm fails detecting a (tangential) perturbation that causes a fall; neither the NNGI deviates from the RLC, nor the D-statistic increments its value. On the contrary, if the designer chooses an ECN too short, the algorithm can provide false detections, as it does in Fig. 5a, b when $m = 30$. However for $m \geq 40$ it provides the same results, showing that the robot is walking stably. From the execution of the proposed algorithm with all the available trials, we observe that it achieves an optimal performance (no false detections, and a 100% detections) for a value $m = 50$.

- The threshold on the D-statistic, D_{th} . As said in subsection 2.2 this threshold is an experimental approach to being inside or outside the basin of attraction. If the designer chooses a small value for D_{th} , the algorithm will detect perturbations that could be rejected naturally, but if its too large, it will fail to detect that the robot is being perturbed, or it will not provide a sufficiently fast detection. Again it must be tuned after executing a number of trials with and without perturbations. From the experiments presented in this paper, we conclude that a threshold $D_{th} = 100$ avoids false detections because the highest value of D during normal walking is $D = 60.80$.

Table 1 summarizes the results for different values of m . In the table P stands for a push perturbation and T for a trip, the number represents the trial. After the tuning processed, it is concluded that the value of D_{th} has little influence in the performance of the algorithm compared with m . It only affects the detection delay. Once we have selected a value that avoids false positives during normal walking, the detection delay varies less than 5 ms if $D \leq 2000$.

3.3. Stable walking experiments

First, we executed the algorithm during a series of stable walking trials. As expected, the NNGI tracked

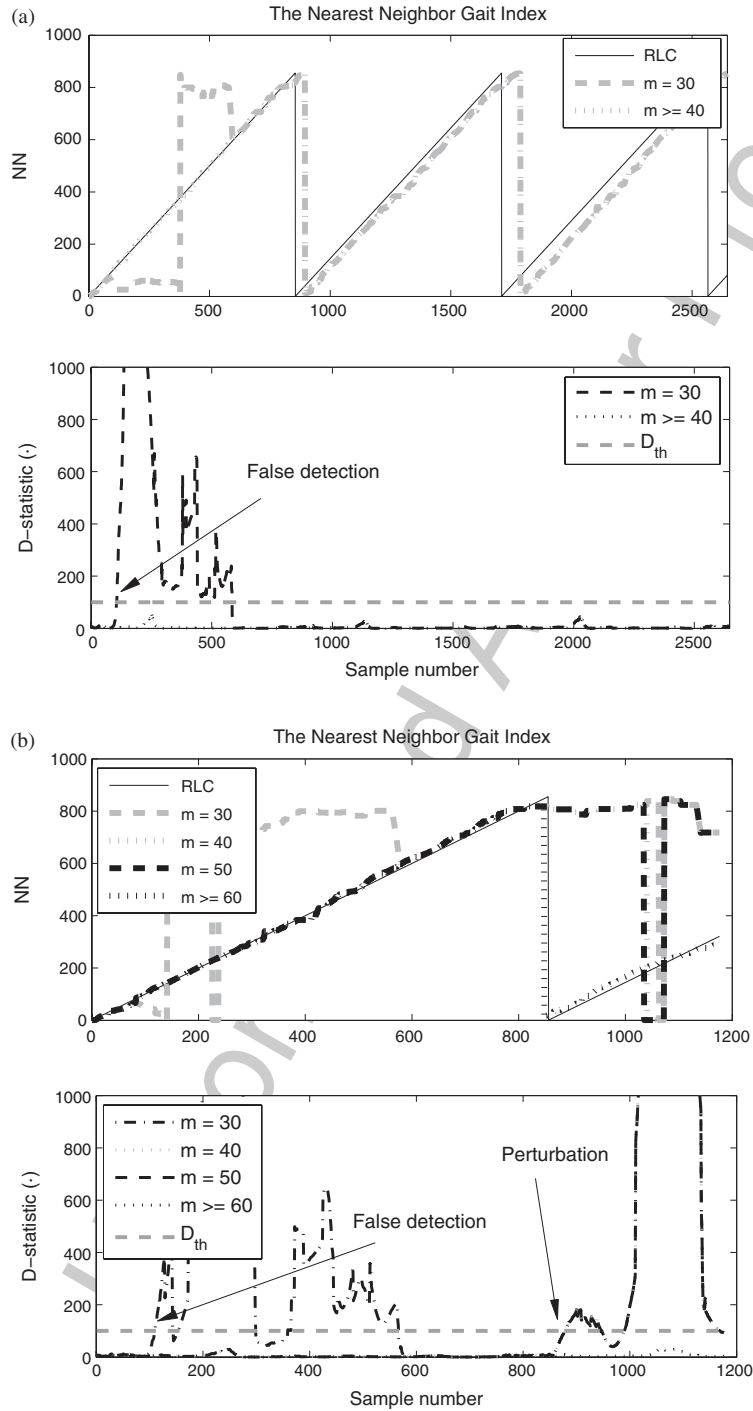


Fig. 5. Selection of the parameters of the algorithm: The length of the Ensemble of Candidate Neighbors, m (top), and the threshold for the D-statistic, D_{th} (bottom). (a) Execution of the NNGI in one stable run of Meta. Top: The solid black line represents the RLC, the NNGI for different values of m is shown as dashed gray lines. Bottom: Dashed and dotted black lines represent different values of m , the dashed gray line the D-statistic. (b) Execution of the NNGI during trip trial 1 (which ended in a fall). Top: The solid black line represents the RLC, the NNGI for different values of m is shown as dashed gray and black lines. Bottom: The four black lines represent different values of m , the dashed gray line the D-statistic.

Table 1
Influence of parameter m perturbation detection performance

| m | False positives | No detection? |
|-----|-----------------------------------|--|
| 30 | Always | Always |
| 40 | P2 ² , T2 ² | – |
| 50 | – | – |
| 60 | – | P3, T1, T3 |
| 70 | – | P1 ¹ , P3, T1, T3, T4 |
| 80 | – | P1 ¹ , P3, P4 ¹ , T1, T3, T4 |
| 100 | – | P1 ¹ , P3, P4 ¹ , T1, T3, T4 |

¹ During the perturbation the D-statistic reaches a peak value not much larger than in normal walking, e.g. below 200. This threatens successful detection.

² The robot suffered a perturbation but did not deviate from its limit cycle, which indicates that it kept inside the basin of attraction.

478 considerably close the RLC, but with subtle differences
 479 in joint trajectories, velocities, and stride duration.
 480 Figure 6 shows an example of how the NNGI and
 481 the D-statistic evolve during three stable strides. It is
 482 observed that the NNGI (dashedline) tracks closely
 483 the RLC, with only negligible deviations, indicating
 484 that the biped is following its RLC. Concerning to
 485 the D-statistic, lower panel in the figure, it presents
 486 peaks of 56.04, 31.34, and 47.74 around samples num-
 487 ber 250, 1100, and 2000 respectively. This corresponds
 488 to the heel strike of the outer legs. Table 2 depicts the
 489 peak values of the D-statistic for 10 stable strides. All

of them appear also when the outer legs impact the
 ground. The reason for this is two fold: First, that the
 synchronization of the outer legs happens just before
 heel strike (originating the most considerable inter-
 stride variation), and second, because of an insufficient
 sampling frequency of the RLC, which does not let the
 algorithm record a state more similar (closer) to the
 current one. Nevertheless, increasing the amount of
 points of the RLC would require an excessive amount
 of memory and computational resources of the onboard
 computer; as said, it is more effective to ignore these
 peaks selecting a value for the D-statistic threshold
 $D_{th} = 100$.

Figure 7 shows the calculation of the NN during the
 whole experiment. It represents the Euclidean distance
 at every point during the walk. As the prototype is walk-
 ing stably the NN follows the RLC, which implies that
 the point with least distance to the current state of the
 walker (solid black line) is always in the neighborhood
 of the expected state, i.e. candidate number 0; thus the
 robot is walking in a limit cycle.

3.4. Perturbed walking experiments

Together with the stable walking experiments, a
 series of trials where the walker suffered a push or

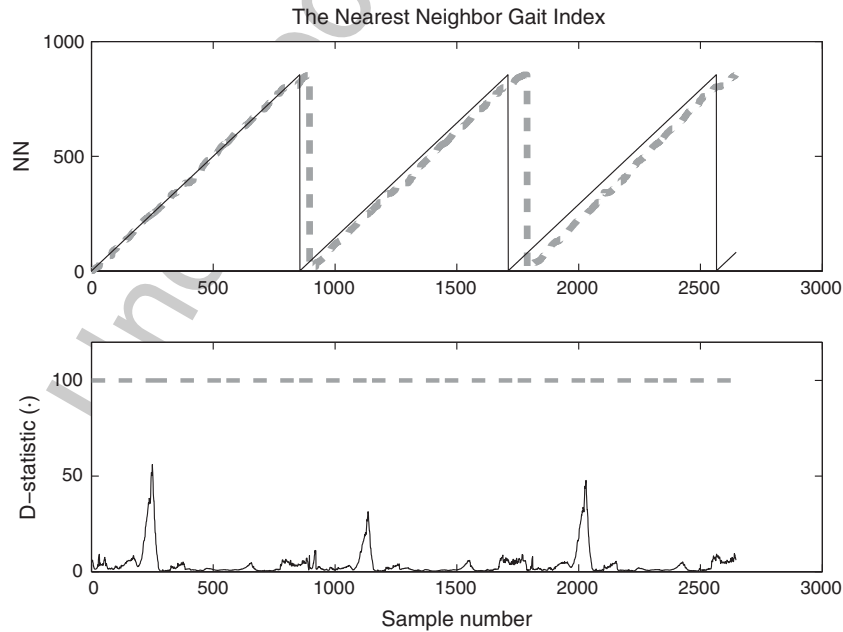


Fig. 6. Upper panel: the dotted line represents the NN for three consecutive stable strides as provided by the NNGI. The solid line corresponds to the RLC, the dashed line to the NNGI. The lower panel shows the D-statistic (solid line) and the selected threshold D_{th} (dashed line).

Table 2
D-statistic for 10 stable walking strides

| | | | | | |
|-----------|-------|-------|-------|-------|-------|
| Stride | 1 | 2 | 3 | 4 | 5 |
| Max(D-st) | 56.04 | 31.34 | 47.74 | 30.04 | 36.96 |
| Stride | 6 | 7 | 8 | 9 | 10 |
| Max(D-st) | 60.80 | 41.07 | 16.09 | 49.76 | 30.64 |

a trip were performed. They served to validate the proposed technique and, as explained before, to select the adequate value for the parameters. Trip experiments consisted in an obstacle made of steel placed on the path of the robot, so that the biped stumbled with it at different gait phases. Pushes were gently applied by an experimenter at the body of the robot, also at different moments in the gait cycle. Figure 8 shows the execution during a push experiment. As a result of the disturbance the walker deviates dramatically from its RLC, as it can be observed in the upper plot; moreover, the D-statistic reaches to a high value, 5600.5, about one hundred times larger than in stable walking. In spite of this, the biped is able to recover from the perturbation by putting its swinging leg quickly on the floor, performing a so-called “lowering strategy” in humans, Forner-Cordero et al. [9]. Table 3 summa-

rizes the peak values of the D-statistic during four trip and push experiments. The D-statistic overpasses the selected threshold ($D_{th} = 100$) for all the experiments in which the robot falls, but it provides three “false alarms” when the robot suffers a push (experiments number 1, 2, and 4). In two of these cases (experiments 1 and 4) the robot almost fails to perform the subsequent ankle push off, which is the major cause of falling in the ensemble of push and trip experiments; therefore it would be preferable to trigger a recovery reaction to avoid a potential fall. This is shown in Fig. 9a where we observe that the ankle angle of the inner leg at push-off after the perturbation is abnormally small (for experiment 1). Experiment 2, on the other hand, exhibits no noticeable differences in leg angles with respect to unperturbed trials, only decreased forward tilt in the stride after the perturbation, Fig. 9b. Since joint angles (the other state variables) follow normal profiles, the D-statistic keeps low values, not indicating the occurrence of the perturbation. Related to experiment 3, the peak in the D-statistic happens 8 milliseconds after the heel strike of the outer legs, thus it could be related to the small peaks that happen at that moment in normal walking but amplified by the push.

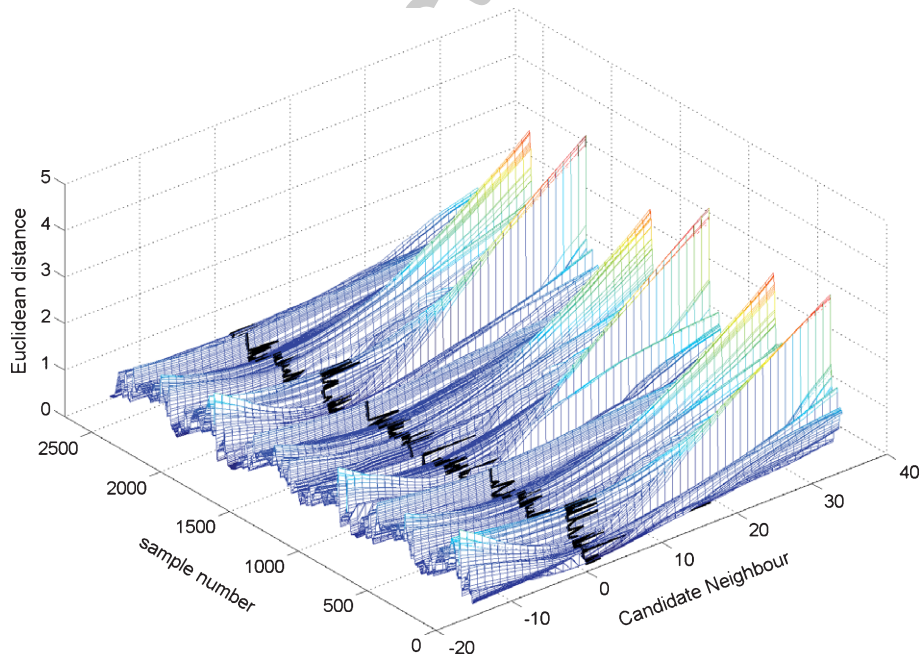


Fig. 7. Calculation of the NN during a stable walking experiment. The surface represents the Euclidean distance to every candidate neighbour at every sample of the trial, the black solid line the NN.

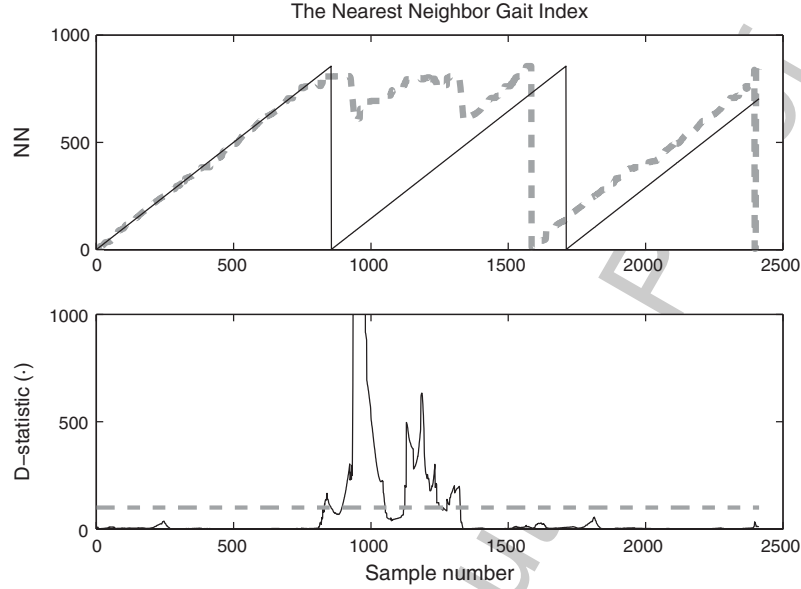


Fig. 8. Upper panel: the dashed line represents the NN for push trial 3 (the robot kept walking) as provided by the NNGI. The solid line corresponds to the RLC, the dashed line to the NNGI. The lower panel shows the D-statistic (solid line) and the selected threshold D_{th} (dashed line).

Table 3
D-statistic for 8 perturbed experiments

| | 1 | 2 | 3 | 4 |
|------------|------------------|-------|------------------|------------------|
| Push trial | 1 | 2 | 3 | 4 |
| Max(D-st) | 5600.5 | 63.17 | 4967.8 | 6227.4 |
| Fall? | No ¹ | No | No | No ¹ |
| Trip trial | 1 | 2 | 3 | 4 |
| Max(D-st) | 18074 | 54.40 | 2523.3 | 6487.0 |
| Fall? | Yes ² | No | Yes ² | Yes ³ |

¹ The robot experiences notable problems to perform ankle push off after the perturbation, but it succeeds.

² The fall is caused because the heel strike after the perturbation is not performed with the legs completely outstretched.

³ Ankle push off after the perturbation is not executed adequately; the walker falls backwards.

4. Discussion

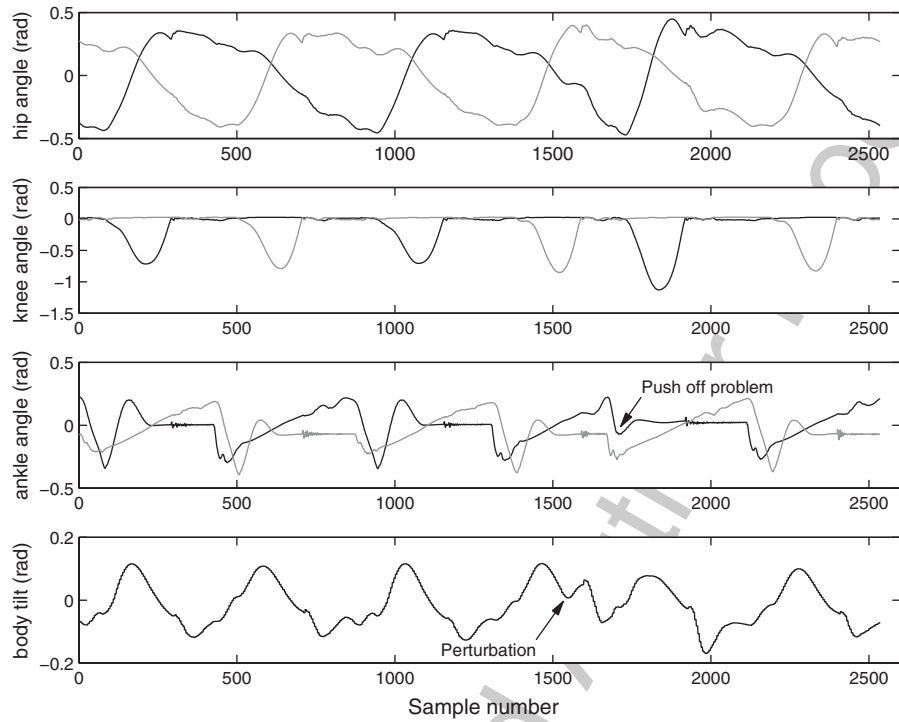
This paper focuses on a new method to monitor the stability of a Limit Cycle Walker based on a normal walker pattern (the RLC) and a static measurement of dynamic stability (the D-statistic). It can be applied not only to detect gait perturbations, but also to quantify dynamic stability. A brief discussion on these topics is provided next.

4.1. Application to perturbation detection

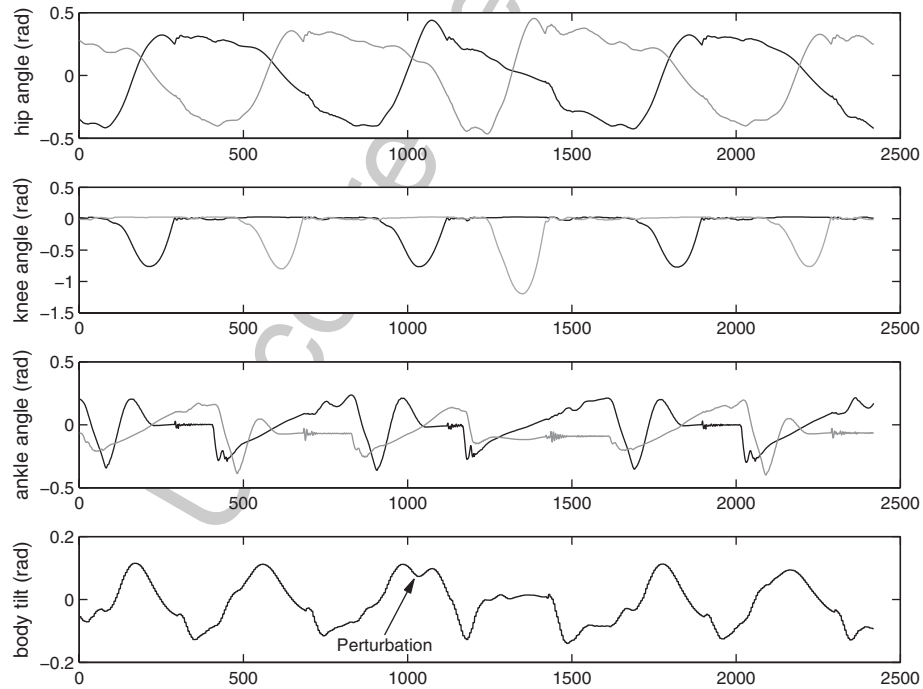
The experimental results presented in Section 3 indicate that the implementation of the proposed algorithm

provides a technique to detect the occurrence of an unexpected event that may lead the robot to a fall. In fact, for the selected set of parameters, the algorithm provides no false detections when the robot is walking stably, and it also has a 100% success rate detecting perturbations that cause a fall. Three pushes (push experiments 1, 3 and 4) that did not make the robot collapse were identified as perturbations, but it was observed that the robot experienced serious difficulties avoiding a backwards fall in the subsequent stride in experiments 1 and 4 and that in experiment 3 the “false alarm” happens because the push amplifies the variations that always happen at heel strike of the outer legs.

Related to the delay in perturbation detection, it must be pointed out that in the current setup the occurrence of the perturbation was recorded with a conventional camera that provides 30 Hz sampling rate. Thus, the moment at which the perturbation happens can be estimated with roughly 17 ms error. This error was partially compensated assuming that the perturbation happens when the monotonic increase in the D-statistic (just before when the perturbation is detected) begins. The average delay was estimated as 45.2 ms (standard deviation 3 ms) therefore comparable to short latency reflexes in humans, typically estimated to be around 35 ms van der Linden et al. [30] Note that humans serve as reference in biomimetic gait control research.



(a) Joint angles during push trial 1.



(b) Joint angles during push trial 2.

Fig. 9. Joint angles (rad) for the hip, knee, ankle, and body tilt during push trials 1 and 2. Data sampled at 500 Hz. The black and grey lines represent the inner and outer legs respectively. The moment at which the perturbation is applied is indicated by an arrow in the body tilt plot.

594 Table 1 summarizes the performance in perturbation
 595 detection based on different values of m . The second
 596 parameter D_{th} only affects in detection time in always
 597 less than 5 ms above the value that avoids false posi-
 598 tives during normal walking (60.80) and below 2000.
 599 Thus it is not thoroughly described. Current work on
 600 the implementation of the NNGI in a new bipedal robot
 601 and its simulation model will provide a more precise
 602 measure of the detection delay and the influence of the
 603 parameters D_{th} and m in the final results.

604 Moreover, we are working on the validation of
 605 our perturbation detection algorithm in the novel
 606 ESBiRRo exoskeleton, a hip-knee-ankle-foot ortho-
 607 sis (HKAFO) based on the concept of Limit Cycle
 608 Walking, Fig. 10. The ESBiRRo exoskeleton consists
 609 of variable stiffness ankle and knee joints and active
 610 hip joints, driven by flat DC motors. Like this, the
 611 exoskeleton has most of the weight distributed prox-
 612 imally, not influencing the subjects dynamics, and
 613 letting the human-robot system settle naturally into
 614 a Limit Cycle.



Fig. 10. Lateral view of ESBiRRo HKAFO exoskeleton depicting DC flat motors at the hip, and variable stiffness actuators at knee and ankle.

4.2. A novel tool to assess dynamic stability

615 Although this paper focuses on perturbation detec-
 616 tion, the core of the proposed method is to provide a
 617 linearized measurement of the dynamic stability of a
 618 walker. As reviewed in the introduction, the stability of
 619 Limit cycle Walkers has been traditionally assessed in a
 620 step-to-step basis, i.e. slicing the limit cycle at one fixed
 621 point (for example at heel strike of a given leg) and cal-
 622 culating the inter-stride variation in this fixed Poincaré
 623 section. The way to measure this variation changes
 624 with the technique; it can be based, for example, on the
 625 calculation of Floquet Multipliers, Hurmuzlu [15], or
 626 on a series of gait indicators, Hobbelen and Wisse [11].
 627 However, these methods ignore what is happening in
 628 all the other states of the gait cycle.

629 The application of the proposed method to a walk-
 630 ing prototype yielded some insight into its inherent
 631 dynamic stability. Notice that the dynamic stability of
 632 the walker is influenced not only by its walking con-
 633 troller, but also by its mechanical design. Our major
 634 discoveries in Meta were: 1) during unperturbed walk-
 635 ing, the largest inter-stride variation happened at heel
 636 strike of the outer legs because of their synchroniza-
 637 tion mechanism, 2) perturbations at mid and late swing
 638 cause a “fast advance” in the tangential direction of the
 639 limit cycle (a so-called lowering strategy in humans
 640 Forner-Cordero et al. [9]), but the robot does not fall
 641 if it can perform a sufficiently powerful ankle push
 642 off afterwards (this agrees with previous experiences
 643 demonstrating the role of ankle push off in walking sta-
 644 bility and energetics, Hobbelen and Wisse [13], Kuo
 645 [19]), and 3) perturbations at early swing make the
 646 robot fall because the swinging legs land not com-
 647 pletely stretched, making the knees collapse. These
 648 results suggest that the application of the NNGI method
 649 may help us to understand how different factors affect
 650 the dynamic stability of a given robot. Moreover, with
 651 help of an adequate benchmark, the NNGI could be
 652 used to compare the stability of different walking
 653 machines or control techniques, measuring how the
 654 same perturbation affects them.

5. Conclusions

655 This paper presents a method for detection of gait
 656 perturbations in bipedal walkers, both humanoid robots
 657 and exoskeletons. The algorithm monitors online the
 658 state of the robot and decides whether a perturbation is
 659
 660

happening based on a phase representation of the normal walking of the biped. It presents the advantages of having low computational cost and avoiding the need of a model of the robot dynamics, just a reference gait pattern. Moreover, the algorithm has only two parameters the designer needs to tune; among them only one has a large influence in the performance of the algorithm, thus it is quickly to adjust. This is done with data from a reduced number of stable and perturbed walking trials. The proposed method was validated with a Limit Cycle Walker prototype providing a 100% success rate in perturbation detection for the current experimental apparatus and adequately tuned parameters, with no false positives when the robot is walking unperturbed. The average delay in disturbance detection is 45ms, comparable to short latency reflexes in humans.

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