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(54) **HIGH TORQUE LIMITED ANGLE COMPACT AND LIGHTWEIGHT ACTUATOR**

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(57) **ABSTRACT**

A high torque limited angle compact and lightweight actuator that comprises a driven pulley (11), a flexible tie-member (6), which is wound about the driven pulley (11), a linear actuator (7) and an inversion mechanism (8). In particular, the linear actuator (7), which is located with respect to the driven pulley (11) such that the direction is substantially tangential to it, comprises a movable element (10) that carries out a linear movement along a line according to two opposite directions (10'), (10''). The inversion mechanism is such that when an input portion (8') moves along a line (first straight line), tangential to the driven pulley, of a certain amount an output portion (8'') moves along another line (second straight line), which is also tangential to the driven pulley, for a same movement amount, such that the total length of the tie-member (6) is unchanged. (FIG. 2)

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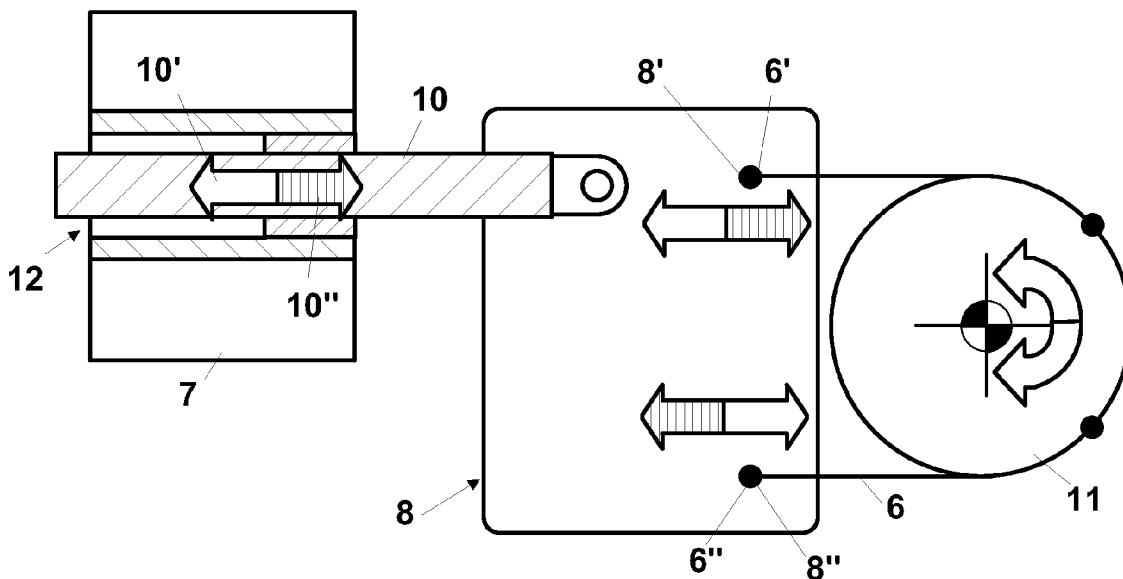
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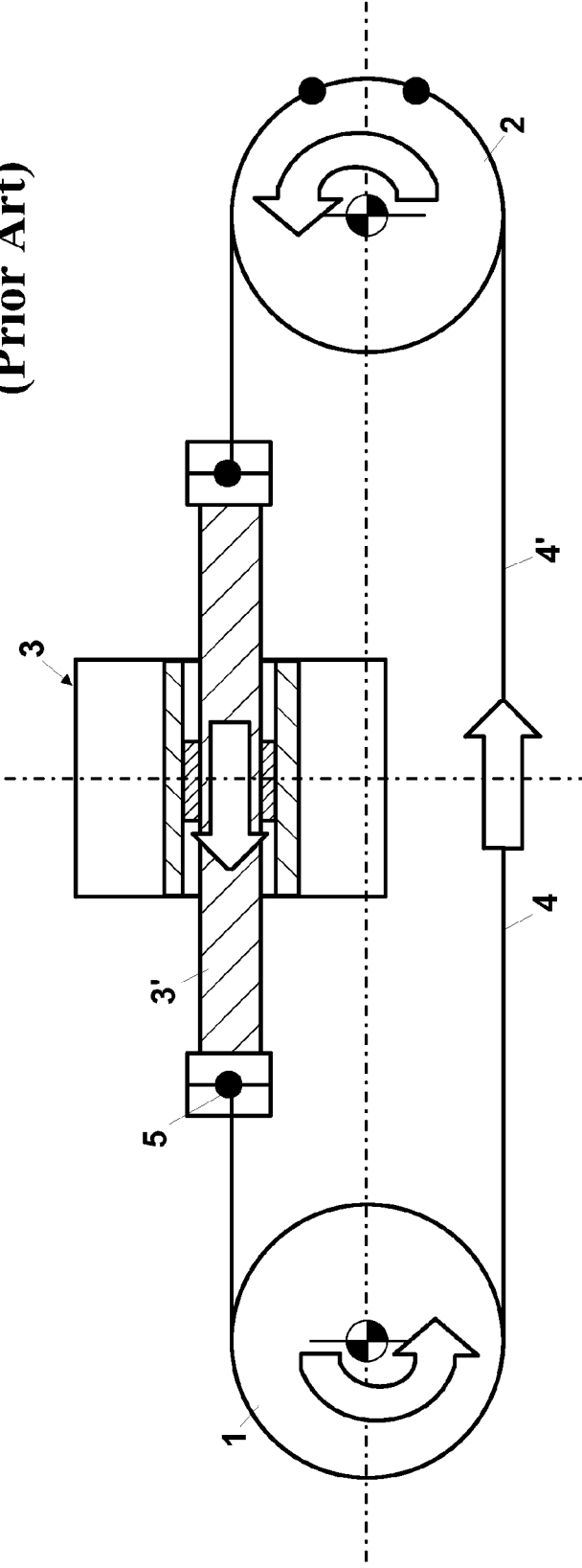
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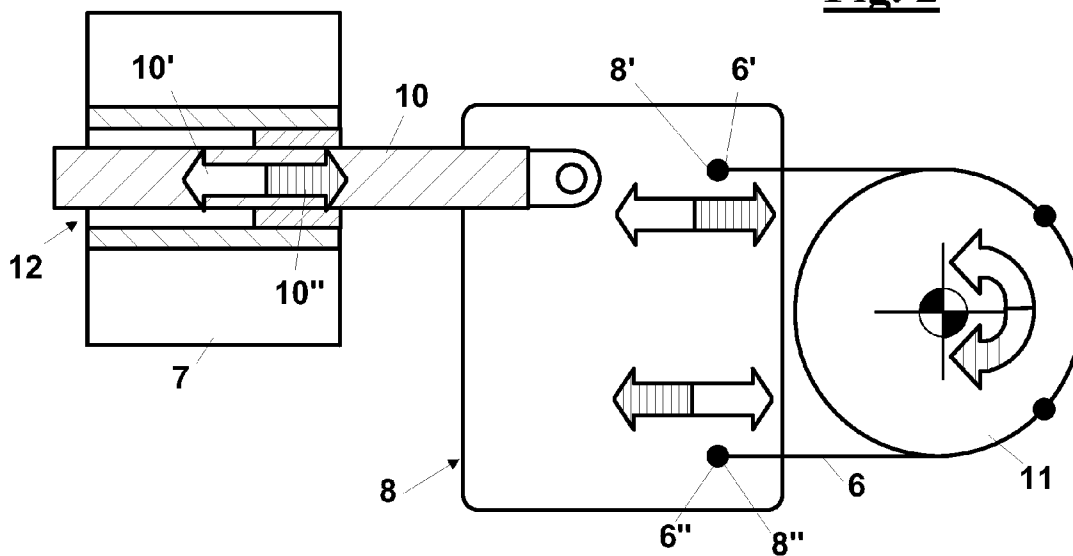
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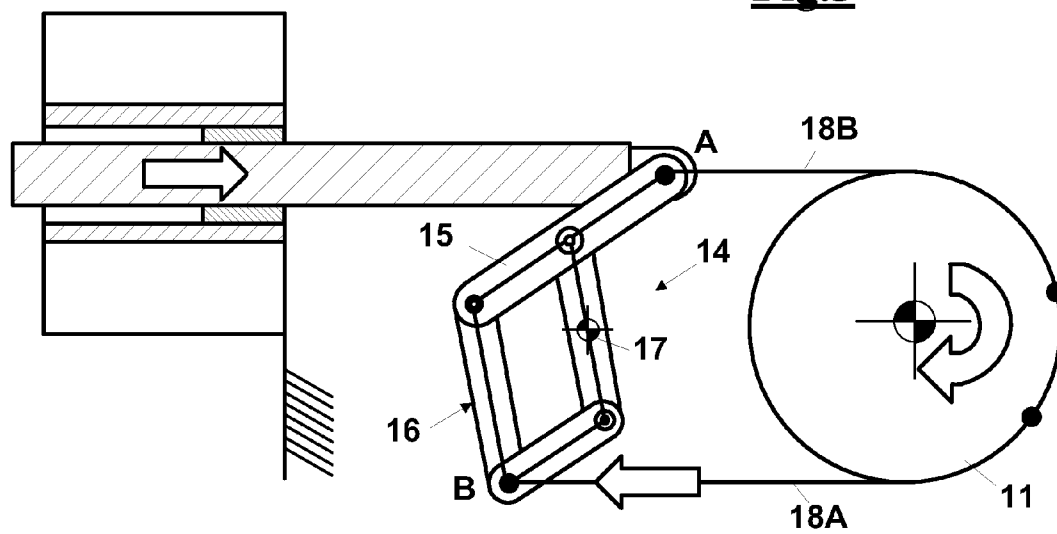
**Fig. 1**  
**(Prior Art)**



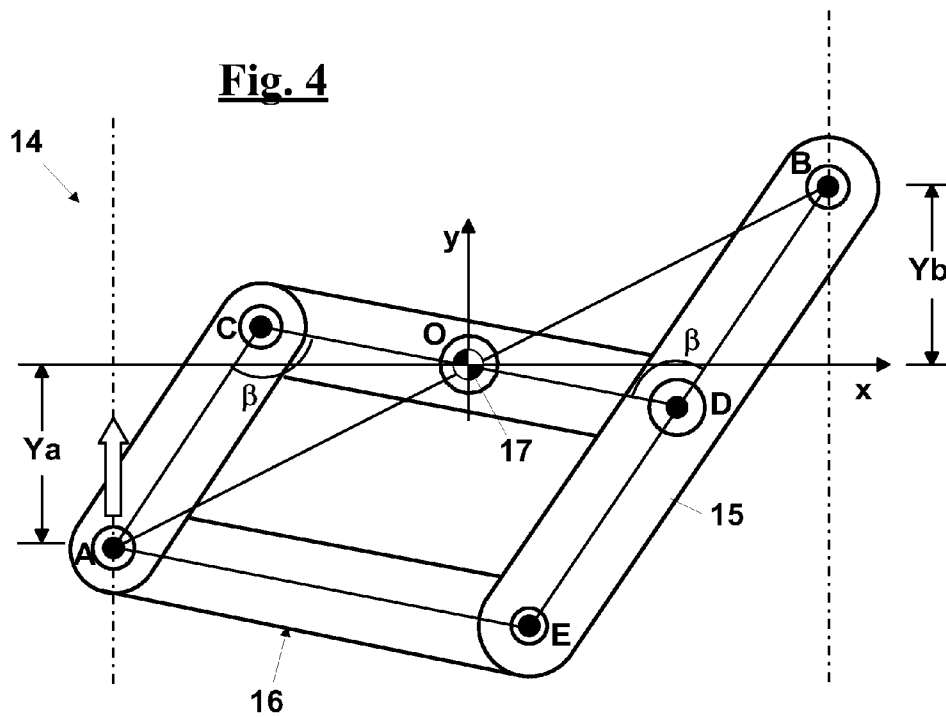
**Fig. 2**



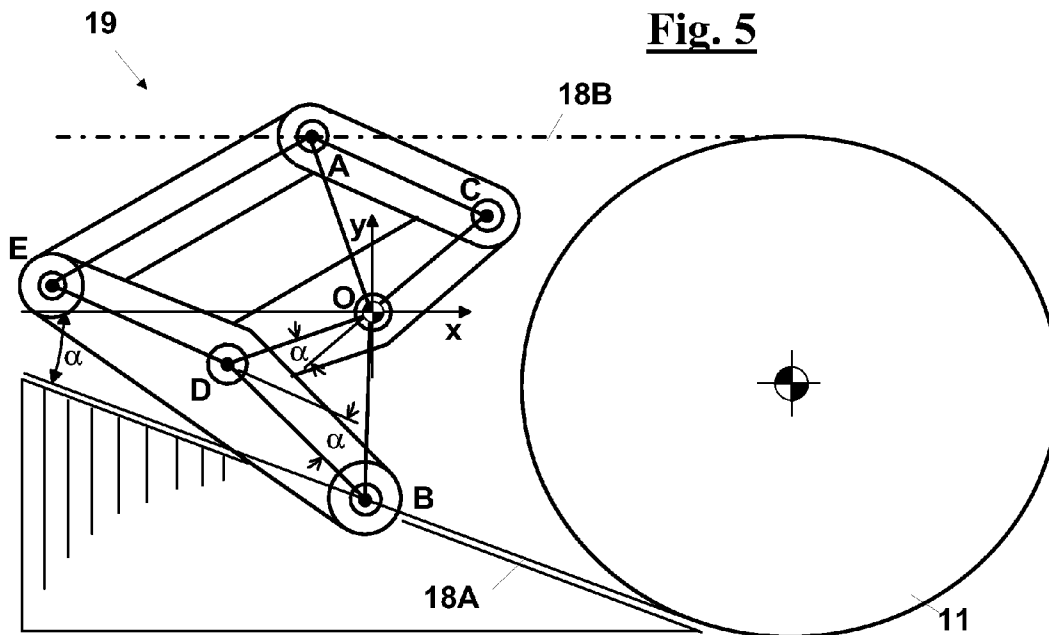
**Fig.3**



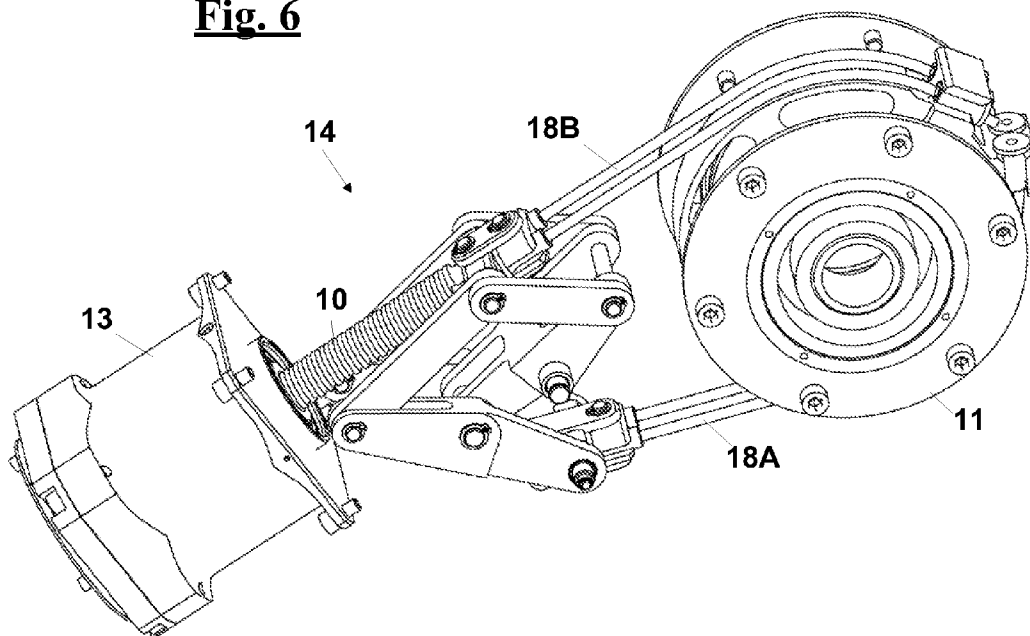
**Fig. 4**



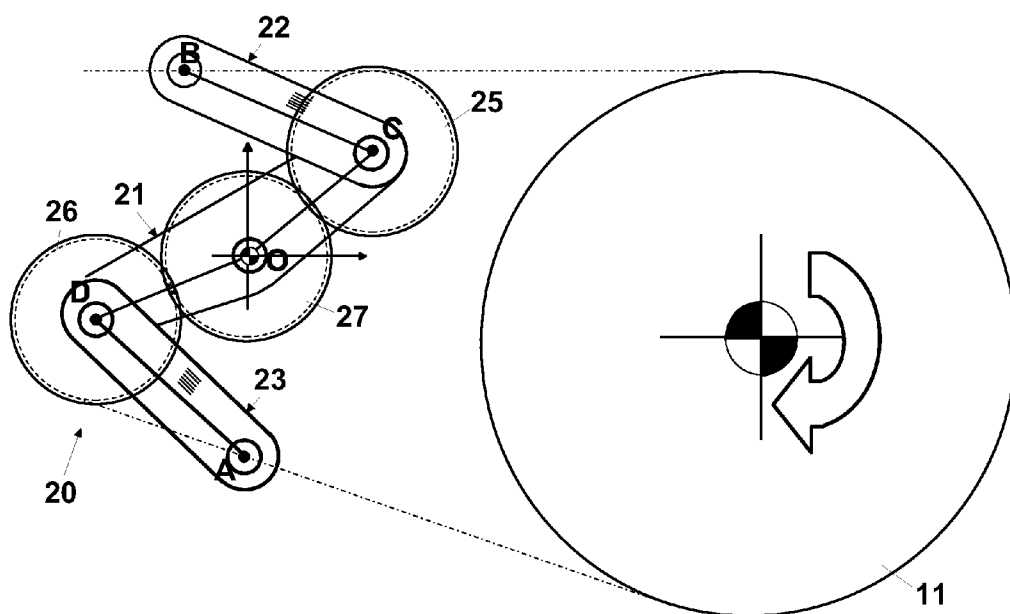
**Fig. 5**

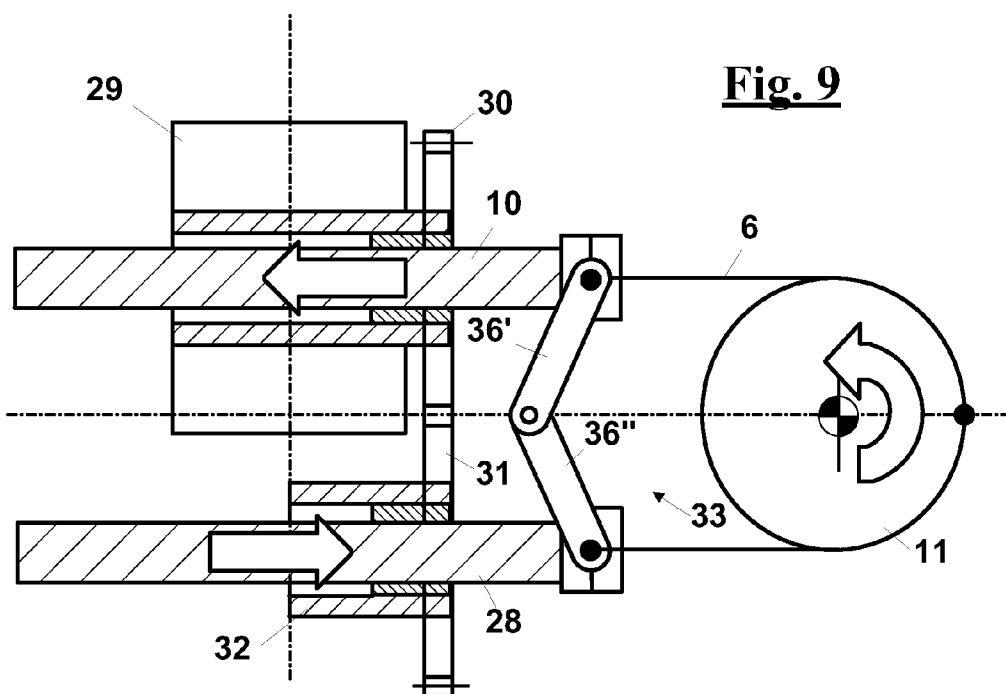
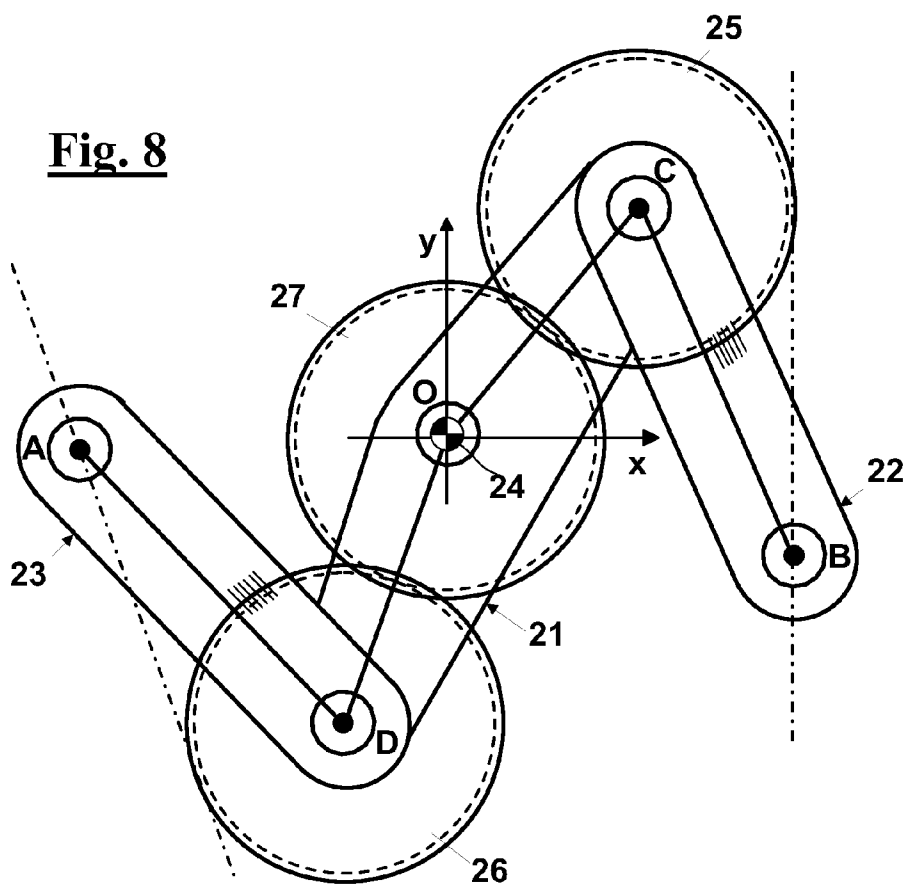


**Fig. 6**



**Fig. 7**





**HIGH TORQUE LIMITED ANGLE COMPACT AND LIGHTWEIGHT ACTUATOR**

**FIELD OF THE INVENTION**

[0001] The present invention relates to robotics and, in particular, it relates to a new type of actuator that can be implemented of various types of robot, such as haptic interfaces, used in Virtual Reality Systems (VRS) and in Tele-Operation Systems (TOS) or, still, Exoskeletons for Human Performances Augmentation, EHPA. Other possible application fields are Active Prostheses and Orthoses as well as Rehabilitation Robotics.

[0002] The usability and performances of all these types of robotic appliances are mainly determined by the mechanical features of the actuators that are necessary for their implementation. In particular, actuators are desirable with high torque/weight ratio, torque/size ratio, high mechanical efficiency, low friction and limited play

**DESCRIPTION OF THE PRIOR ART**

[0003] The actuators in engineering are transducers that are capable of transforming an input variable, normally electric, into a mechanical movement. Some examples of actuators are parts of a robot that interact with external systems as well as gripping mechanisms, mechanical arms and other moving parts.

[0004] In the prior art many actuator devices are provided, that are mainly comprised of an electric, pneumatic or hydraulic motor, by a reduction unit and by a mechanical transmission.

[0005] The use of a reduction unit in the implementation of actuators allows to augment the torque/weight and torque/size ratios, but with the disadvantage of reducing mechanical efficiency and increasing friction and mechanical play.

[0006] Among the various known techniques of mechanical reduction, the ball nut screw allows obtaining the better performances. In fact, the weight of the reduction unit is remarkably more limited, and a mechanical efficiency that is relatively higher and a friction and backlash sensibly lower or even near to zero are obtained.

[0007] Such technique allows obtaining actuators with limited angular span, however enough to meet the requirements of the previously cited robotic applications in the field of the present invention. An additional problem that affects this technique with respect to the other (for example epicyclic reduction gears), is that the movement of the screw has to be converted from linear to rotational. This conversion can be effected simply using tendons and idle and driven pulleys.

[0008] With reference, for example, to WO2004/083683, an actuator device is described comprising an electric motor, a reduction ball nut screw unit, two pulleys, two tendons, and guides that prevent the rotation of the screw on its own axis. The axis of the first pulley, which is a driven pulley, is coincident to the output axis of the actuator, whereas the second pulley, which is an idle pulley, is arranged opposite to the driven pulley. The first cable is connected to a first end of the screw as well as it is directly connected to the driven pulley, whereas the second cable is wound on the idle pulley and it is connected to the other end of the screw and it is connected also to the driven pulley.

[0009] This way, the driven pulley is caused to rotate when one of the two tendons of the transmission is pulled by the ball nut screw. When the screw translates, for example towards

left, the first cable of the transmission is stretched and the driven pulley rotates in a counterclockwise direction. Similarly, a translation towards the right of the screw the second cable of the transmission is stretched, causing the rotation in a clockwise direction of the driven pulley.

[0010] Such solution, with a single motor/reduction gear screw, develops torques in both clockwise and counterclockwise rotation directions.

[0011] This device, however has the drawback of a relatively high longitudinal encumbrance that is as much greater as the translation stroke of the screw and the radius of the pulleys increase.

[0012] In turn the size is directly responsive to the mechanical requirements of the actuator: maximum torque demand at the output axis and angular travel. With a same electric motor and ball nut screw, the longitudinal encumbrance of the actuator increases as these requirements increase.

[0013] A reduction of the longitudinal encumbrance of the actuators is a desirable goal in the implementation of the cited robot types, in order to achieve kinematical implementations that are isomorphous with respect to the physiological features of the human limbs.

**SUMMARY OF THE INVENTION**

[0014] It is a feature of the present invention to provide an actuator with torque/weight and torque/size ratios that are improved with respect to the prior art.

[0015] It is also a feature of the present invention to provide an actuator that presents a high mechanical efficiency and low friction.

[0016] It is a further feature of the present invention to provide an actuator that has a high structural stiffness as well as a close to zero mechanical play. These and other objects are achieved by an actuator that is adapted to provide a rotation and a torque as an output, comprising:

[0017] a driven pulley;

[0018] a flexible tie-member, wherein said tie-member is wound in part about said driven pulley and has a first and a second tie-member portions that have respectively a first and a second ends;

[0019] a linear actuator that has a movable element that is adapted to provide a movement according to two opposite directions;

[0020] an inversion mechanism that is connected to said movable element, said inversion mechanism having:

[0021] an input portion that is connected to said movable element and to said first end of said flexible tie-member,

[0022] an output portion that is connected to said second end of said flexible tie-member;

[0023] said inversion mechanism being such that

[0024] when said movable element moves in said first direction an input pull movement is created of said first tie-member portion that provides a torque action to said pulley in a first rotation direction, with said output portion that effects a compliant output movement for carrying said second tie-member portion, and

[0025] when said movable element moves in said second direction, an output pull movement is created of said second tie-member portion that provides a torque action to said pulley in a second rotation direction that is opposite to said first rotation direction, such that said input portion effects an input movement that follows said movable element in a compliant way for carrying said first tie-member portion.

**[0026]** Advantageously, said linear actuator has said movable element that is adapted to provide a movement along a line according to two opposite directions and mounted with respect to said driven pulley such that said line is substantially tangential to said driven pulley, said inversion mechanism being such that when said input portion is moved along said line (input straight line) for a determined movement amount, said output portion is moved along another line (output straight line), which is also substantially tangential to said pulley, for a same movement amount.

**[0027]** In particular, when said input portion is moved along said straight line, the total length of said flexible tie-member is unchanged.

**[0028]** Advantageously, said tie-member portion, which is wound about said driven pulley, is connected to said driven pulley.

**[0029]** In a possible embodiment of the invention, said tie-member portion that is wound about said pulley is discontinued and connected to said driven pulley in two respective discontinuation points.

**[0030]** Preferably, said linear actuator comprises:

**[0031]** a rotational motor that is adapted to provide a circular movement;

**[0032]** a reduction unit that is adapted to receive said circular movement and to turn it into a linear movement;

**[0033]** a mechanical transmission that transfers said linear movement to said movable element.

**[0034]** Preferably, said reduction unit is a ball nut/screw device, which is suitable to ensure less rolling resistance between the screw and the nut, as well as to ensure a high mechanical efficiency and minimum play, up to zero, in the two movement directions of said movable element.

**[0035]** Advantageously, said rotational motor is an electric hollow torque motor that has a high torque/weight and torque/size ratios and is such that it allows an easy integration with said nut/screw reduction device is achieved.

**[0036]** Advantageously, said inversion mechanism, in a first exemplary embodiment, is a pantograph mechanism comprising a support arm and a four-bar linkage, wherein an end of said arm forms said input portion and a vertex of said pantograph, opposite to said end, forms said output portion.

**[0037]** In particular, said pantograph mechanism is pivotally connected to the fixed structure (frame) of the actuator at a point that is located on a base bar of said four-bar linkage and on the junction between said vertex of said pantograph and said end of said arm.

**[0038]** Preferably, said inversion mechanism, in a second exemplary embodiment, comprises:

**[0039]** a gear train consisting of a first and a second gears, having a same primitive radius, connected indirectly by an intermediate gear, a stiff support to which said gears are pivotally connected, a first arm that is integral to said first gear and a second arm that is integral to said second gear, said first and second arm having respective ends that forms said input portion and said output portion of said inversion mechanism.

**[0040]** Preferably, said gears are straight-cut gears.

**[0041]** Advantageously, said inversion mechanism, in a third exemplary embodiment comprises:

**[0042]** a auxiliary movable element that has a movement that is opposite to said movable element, said opposite movement of said auxiliary movable element being

obtained directly from said motor, wherein said auxiliary movable element forms said output portion of said inversion mechanism.

**[0043]** Advantageously, said opposite movement of said auxiliary movable element is obtained directly from said motor by means:

**[0044]** a first gear that is adapted to pick up said circular movement from said motor;

**[0045]** a second gear that meshes with said first gears,

**[0046]** a nut/screw coupling between said second gear and said auxiliary movable element.

**[0047]** Advantageously, said movable element and said auxiliary movable element are connected to each other by an antirotation device that blocks a rotation of the screws about their own axis.

**[0048]** In particular, said antirotation device comprises two stiff links, each having a first and a second ends, said links pivotally connected to each other at said first end and pivotally connected to said movable element and said auxiliary movable element at said second ends.

**[0049]** Advantageously, said auxiliary movable element has a movement that is opposite to said movable element such that if said movable element moves according to said first or according to said second direction of a measured amount, said auxiliary movable element moves in an opposite direction according to a same movement amount.

**[0050]** In a possible exemplary embodiment, said input and output lines, along which said input portion and output portion of the inversion mechanism move, are parallel to each other.

**[0051]** In a preferred exemplary embodiment, said input and output lines are at a predetermined angle with respect to each other, such that they cross each other at a point that is located at a same side of said inversion mechanism with respect to said pulley.

**[0052]** Advantageously, said first and second line form an angle that is set between 5 and 45°, preferably between 10 and 35°, in particular about 20 and 30°. This way, the transversal size of the actuator is sensibly low.

#### BRIEF DESCRIPTION OF THE DRAWINGS

**[0053]** The invention will be made clearer with the following description of an exemplary embodiment thereof, exemplifying but not limitative, with reference to the attached drawings in which:

**[0054]** FIG. 1 shows an double pulley actuating device, according to the prior art;

**[0055]** FIG. 2 shows a diagrammatical general view of the high torque compact actuator, according to the invention;

**[0056]** FIG. 3 shows a first exemplary embodiment that adopts as inversion mechanism a pantograph device;

**[0057]** FIG. 4 shows a diagrammatical operative view of the actuator with the pantograph mechanism of FIG. 3;

**[0058]** FIG. 5 shows an exemplary embodiment of the pantograph mechanism of FIG. 4;

**[0059]** FIG. 6 shows a perspective view of limited angle and high torque compact actuator, with a pantograph mechanism, according to the invention;

**[0060]** FIG. 7 diagrammatically shows a second exemplary embodiment of the actuator that uses, as inversion mechanism, a gear mechanism;

**[0061]** FIG. 8 shows, in detail the gear mechanism of FIG. 7;



[0062] FIG. 9 shows a third exemplary embodiment of the inversion mechanism that adopts a second nut/screw device.

DETAILED DESCRIPTION OF SOME EXEMPLARY EMBODIMENTS

[0063] With reference to FIG. 1, an actuator is shown according to the prior art, which comprises mainly a first pulley 1 and a second 2 pulley, a motor 3, a ball nut/screw device 5 and two branches of tendons 4 and 4' that allow to transfer the movement in both rotation directions of the pulleys. In particular, the axis of pulley 2, which is a driven pulley, is coincident to the output axis of the actuator, whereas the pulley 1, which is an idle pulley, is arranged on the rear part of a motor/reduction gear. The first portion, or branch, of tendon 4 is connected to one end of the ball nut/screw device 5, as well as it is directly connected to driven pulley 2, whereas the second portion, or branch, of tendon 4' is wound on idle pulley 1 and it is connected to the second end of the ball nut/screw device and, also, to driven pulley 2.

[0064] This way, driven pulley 2 is caused to rotate in a clockwise, or counterclockwise, direction, according to which of the two tendons 4 and 4' of the transmission is pulled. For example by moving screw 3' towards left, branch 4 of the transmission is stretched such that driven pulley 2 is caused to rotate in a counterclockwise direction. Vice-versa, a movement towards the right of the screw causes second branch 4' of the transmission to be stretched such that driven pulley 2 rotates in a clockwise direction. Additional devices, in a way not shown in FIG. 1, are necessary for avoiding the rotation of the screw about its own axis.

[0065] FIG. 2 shows a diagrammatical view of a rotational actuator, according to the invention, that is adapted to transmit to the output axis a high torque for a limited angular travel.

[0066] More specifically, the actuator comprises a driven pulley 11, a flexible tie-member 6, which is wound about driven pulley 11, a linear actuator 7 and an inversion mechanism 8. In detail, flexible tie-member 6 is wound about driven pulley 11 and it has a first and a second tie-member portions that have respectively a first 6' and a second 6'' end.

[0067] According to the invention, linear actuator 7 has a movable element 10 that carries out a linear movement along a line according to two opposite directions 10' and 10''. Linear actuator 7 is located with respect to driven pulley 11 such that the line is substantially tangential to driven pulley 11.

[0068] As shown in FIG. 2, inversion mechanism 8 has an input portion 8' that is connected to the movable element 10 and to the first end 6' of flexible tie-member 6, and an output portion 8'' that is connected to the second end 6'' of said flexible tie-member.

[0069] The inversion mechanism is such that when input portion 8' moves along a line (first straight line), which is tangential to the driven pulley, for a certain amount the output portion 8'' moves along another line (second straight line), which is also tangential to the driven pulley, for a same movement amount, such that the total length of tie-member 6 is unchanged.

[0070] In particular, when the linear actuator moves in direction 10', the first portion of flexible tie-member 6 is stretched, driven pulley 11 rotates in a counterclockwise direction and the inversion mechanism is not loaded. Vice-versa, when the linear actuator moves in direction 10'', the second portion of the flexible tie-member is stretched, driven

pulley 11 rotates in a clockwise direction and the mechanism is loaded by the forces of the transmission.

[0071] Always with reference to FIG. 2, linear actuator 10 comprises a rotational motor (visible in FIG. 6) that is adapted to provide a circular movement, a reduction unit that is adapted to receive the circular movement by the motor turning it into a linear movement, and a mechanical transmission that transfers the linear movement to the movable element 10.

[0072] In particular, the reduction unit is a ball nut/screw device 12, which is suitable to maximally reduce friction between screw and nut, and to obtain a high mechanical efficiency and a low mechanical play, up to zero. Furthermore, rotational motor 13 (visible in FIG. 6), according to a preferred exemplary embodiment is an electric Hollow Torque Motor, which has a high torque/weight and torque/size ratios such that it allows an easy integration with the nut/screw reduction device.

[0073] FIG. 3 shows inversion mechanism 8 in a first exemplary embodiment, which consists of a pantograph mechanism 14 comprising a support arm 15 and a four-bar linkage 16, in which an end A of arm 15 forms input portion 8' of the inversion mechanism and a vertex B of pantograph 16, opposite to end A, forms output portion 8'' of the inversion mechanism (diagrammatically visible in FIG. 2).

[0074] The pantograph mechanism is pivotally connected to the fixed structure of the actuator (frame) at hinge 17, which is located on a base bar of four-bar linkage 16 and, in particular at the junction between the vertex of the pantograph B, which forms output portion 8'', and end A of arm 15, which forms input portion 8'.

[0075] As shown in FIG. 3, the two portions 18A and 18B of the flexible tie-member are connected to driven pulley 11 and to points an and B of the pantograph 14.

[0076] FIG. 4 shows, in detail, the pantograph mechanism 14.

[0077] The articulation hinges of the pantograph are located such that it is  $OD=OC$  and  $CA=DB$ . Owing to the features of pantograph 16, the angle formed between the segments OD and DB is equal to the angle consisting of segments OC and CA (indicated as  $\beta$  in FIG. 4), so that triangles OCA and ODB are equal to each other. Therefore, if point A is moved according to direction Y for an amount Ya, point B is moved according to direction Y for a same movement amount Yb, but in the opposite direction, i.e. it is  $Yb=Ya$ . Similarly, if point A is moved in a direction x for a same movement amount Xa, point B is moved in a direction X for a same movement amount Xb, but in an opposite direction, i.e. it is  $Xb=Xa$ . According to this geometric feature, if an external force is applied to point A, in order to achieve a static balance of mechanism 14 it is necessary to apply another force on point B with the following force components:  $F_{Bx}=-F_{Ax}$  and  $F_{By}=-F_{Ay}$ .

[0078] With respect to the prior art, this solution allows to minimize remarkably the longitudinal encumbrance of the actuator. Another advantage is that the additional mechanisms for avoiding the rotation of the screw are not necessary, owing to the planar kinematics of the pantograph.

[0079] With reference to FIG. 5, an exemplary embodiment is shown 19 of the pantograph mechanism that allows a reduction of the transversal size. In particular, as indicated in FIG. 5, a different configuration of the hinges of the mechanism allows to put an angle a between adjacent segments OD and OC, and between adjacent segments DE and DB, always maintaining  $OD=OC$  and  $AC=DB$ . If quadrilateral DCAE is

still a pantograph, i.e.  $DC=AE$  and still  $AC=DE$ , triangles  $ODB$  and  $ACO$  are still equal. The result of this change is that if point A moves along a straight line, point B moves still along a line, which now is at an angle  $\alpha$  with respect to the other line. The main advantage of this configuration is a sensitive reduction of the transversal size of the actuator. Furthermore, it is possible to provide actuators with angular span larger than  $180^\circ$ .

[0080] Concerning the size of the mechanical components of the inversion mechanism, in a way referred to the size of the driven pulley, it is possible to achieve inclinations between the two lines of  $45^\circ$  and more, even if inclinations between  $20^\circ$  and  $30^\circ$  degrees are preferable.

[0081] With reference to FIG. 6 a perspective view is shown of an exemplary embodiment of the actuator, according to the invention, which adopts as inversion mechanism the pantograph device. In particular, the electric motor 13, and the screw 10 that translates along a line tangential to the driven pulley are shown. Furthermore, FIG. 6 shows the pantograph mechanism 14 and the two branches of tendons 18A and 18B that are wound on driven pulley 11.

[0082] FIG. 7 shows a second exemplary embodiment of the inversion mechanism, consisting of a gear mechanism 20 that is formed, in detail, by a first gear 25 and by a second gear 26, having a same primitive radius and connected indirectly by an gear idle 27 and by a stiff support 21 to which the gears are pivotally connected. Furthermore, mechanism 20 comprises a first arm 22, which is integral to first gear 25, and a second arm 23, which is integral to the second gear 26. In particular, the end of the first and second arm 22 and 23 form, respectively, the input and the output portions of the inversion mechanism.

[0083] According to a preferred exemplary embodiment the gearing 25, 26 and 27 are straight-cut gears.

[0084] FIG. 8 shows, in an enlarged view, the inversion gear mechanism of FIG. 7. This solution has, also, a point connected to the fixed structure of the actuator and, furthermore, the lengths of the connections allow to achieve the same conditions of the pantograph mechanism as it is described above. Owing to these conditions, triangles  $ODA$  and  $OCB$  are still equal. Also this exemplary embodiment allows obtaining movements of the output portion on a line that is at an angle with respect to the line on which is moved the input portion moves, respecting the basic condition that the movement of output portion B is identical and opposite to the movement of input portion A. Furthermore, mechanism 20 has performances that are comparable, versus side and longitudinal size, to the pantograph mechanism of FIG. 3.

[0085] With reference, finally, to FIG. 9 a third exemplary embodiment is shown of the inversion mechanism.

[0086] In particular, it comprises an auxiliary movable element 28 having a movement that is opposite to that of movable element 10 and according to which the opposite movement of auxiliary movable element 28 is obtained directly by the motor 29 and where auxiliary movable element 28 forms the output portion 8" of the inversion mechanism (diagrammatically visible in FIG. 3).

[0087] As shown in FIG. 9, the opposite movement of auxiliary movable element 28 is obtained directly by motor 29 through a first gear 30 that is adapted to get the circular movement from motor 29. The mechanism, furthermore, comprises a second gear 31, which meshes with the first gear 30 and a nut screw coupling 32 between the second gear 31 and auxiliary movable element 28.

[0088] Furthermore, movable element 10 and auxiliary movable element 28 are connected to each other by an anti-rotation mechanism 33 that blocks a rotation of the screws about their own axis.

[0089] In particular, said antirotation mechanism 33 comprises two stiff links 36' and 36", each having a first and a second ends, said links pivotally connected to each other at the first end and pivotally connected to the movable element 10 and to auxiliary movable element 28 at their second ends.

[0090] The foregoing description of a specific embodiment will so fully reveal the invention according to the conceptual point of view, so that others, by applying current knowledge, will be able to modify and/or adapt for various applications such an embodiment without further research and without parting from the invention, and it is therefore to be understood that such adaptations and modifications will have to be considered as equivalent to the specific embodiment. The means and the materials to realise the different functions described herein could have a different nature without, for this reason, departing from the field of the invention. It is to be understood that the phraseology or terminology employed herein is for the purpose of description and not of limitation.

1. An actuator that is adapted to provide a rotation and a torque as an output, comprising:

- a driven pulley;
- a flexible tie-member, wherein said tie-member is wound in part about said driven pulley and has a first and a second tie-member portions that have respectively a first and a second ends;
- a linear actuator that has a movable element which is adapted to provide a movement according to two opposite directions;
- an inversion mechanism that is connected to said movable element, said inversion mechanism having:
  - an input portion that is connected to said movable element and to said first end of said flexible tie-member,
  - an output portion that is connected to said second end of said flexible tie-member;

said inversion mechanism being such that:

- when said movable element moves in said first direction an input pull movement is created of said first tie-member portion that provides a torque action to said pulley in a first rotation direction, with said output portion that effects a compliant output movement for carrying said second tie-member portion, and
- when said movable element moves in said second direction, an output pull movement is created of said second tie-member portion that provides a torque action to said pulley in a second rotation direction that is opposite to said first rotation direction, such that said input portion effects an input movement that follows said movable element in a compliant way for carrying said first tie-member portion.

2. An actuator, according to claim 1, wherein said linear actuator has said movable element that is adapted to provide a movement along a line according to two opposite directions and mounted with respect to said driven pulley such that said line is substantially tangential to said driven pulley, said inversion mechanism being such that when said input portion is moved along said line (input straight line) for a determined movement amount, said output portion is moved along another line (output straight line), which is also substantially tangential to said pulley, for a same movement amount.

3. An actuator, according to claim 1, wherein when said input portion is moved along said straight line, the total length of said flexible tie-member is unchanged.

4. An actuator, according to claim 1, wherein said tie-member portion which is wound about said driven pulley is connected to said driven pulley.

5. An actuator, according to claim 1, wherein said tie-member portion that is wound about said pulley is discontinued and connected to said driven pulley in two respective discontinuation points.

6. An actuator, according to claim 1, wherein said linear actuator comprises:

- a rotational motor that is adapted to provide a circular movement;
- a reduction unit that is adapted to receive said circular movement and to turn it into a linear movement;
- a mechanical transmission that transfers said linear movement to said movable element.

7. An actuator, according to claim 6, wherein said reduction unit is a ball nut/screw device, which is suitable to ensure less rolling resistance between the screw and the nut, as well as to ensure a high mechanical efficiency and minimum play, up to zero, in the two movement directions of said movable element.

8. An actuator, according to claim 6, wherein said rotational motor is an electric hollow torque motor, which has high torque/weight and torque/size ratios such that an easy integration with said nut/screw reduction device is achieved.

9. An actuator, according to claim 1, wherein said inversion mechanism is a pantograph mechanism comprising a support arm and a four-bar linkage, wherein an end of said arm forms said input portion and a vertex of said pantograph, opposite to said end, forms said output portion and wherein said pantograph mechanism is pivotally connected to the fixed structure of the actuator (frame) at a point that is located on a base bar of said four-bar linkage and on the junction between said vertex of said pantograph and said end of said arm.

10. An actuator, according to claim 1, wherein said inversion mechanism, in a second exemplary embodiment, comprises:

- a gear train consisting of a first and a second gears, having a same primitive radius, connected indirectly by an intermediate gear, a stiff support to which said gears are pivotally connected, a first arm that is integral to said

first gear and a second arm that is integral to said second gear, said first and second arm having respective ends that forms said input portion and said output portion of said inversion mechanism.

11. An actuator, according to claim 10, wherein said gears are straight-cut gears.

12. An actuator, according to claim 1, wherein said inversion mechanism, in a third exemplary embodiment, comprises:

- an auxiliary movable element that has a movement that is opposite to said movable element, said opposite movement of said auxiliary movable element being obtained directly from said motor, wherein said auxiliary movable element forms said output portion of said inversion mechanism.

13. An actuator, according to claim 12, wherein said opposite movement of said auxiliary movable element is obtained directly from said motor by means of:

- a first gear that is adapted to pick up said circular movement from said motor;
- a second gear that meshes with said first gears,
- a nut/screw coupling between said second gear and said auxiliary movable element.

14. An actuator, according to claim 12, wherein said movable element and said auxiliary movable element are connected to each other by an antirotation device that blocks a rotation of the screws about their own axis.

15. An actuator, according to claim 14, wherein said antirotation device comprises two stiff links, each having a first and a second ends, said links pivotally connected to each other at said first end and pivotally connected to said movable element and said auxiliary movable element at said second ends.

16. An actuator, according to claim 1, wherein said input and output lines along which said input and output portions of the inversion mechanism are parallel to each other.

17. An actuator, according to claim 1, wherein said input and output lines along which said input and output portions of the inversion mechanism move are at a predetermined angle with respect to each other, such that extensions of such lines cross each other in a point that is located at a same side of said inversion mechanism with respect to said pulley.

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